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Relationship Between Balance Recovery From a Forward Fall and Lower-Limb Rate of Torque Development

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Title Page

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Title:

Relationship between balance recovery from a forward fall and lower-limb rate of torque development

Running head: Balance recovery and rate of torque development

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40 **Abstract**

41 The authors examined the relationship between the maximum recoverable lean angle via
42 the tether-release method with early- or late-phase rate of torque development (RTD)
43 and maximum torque of lower-limb muscle groups in 56 young healthy adults. Maximal
44 isometric torque and RTD at the hip, knee, and ankle were recorded. The RTD at 50-ms
45 intervals up to 250 ms from force onset was calculated. The results of a stepwise
46 multiple regression analysis, early RTD for hip flexion, and knee flexion were chosen as
47 predictive variables for the maximum recoverable lean angle. The present study suggests
48 that some of the early RTD in the lower limb muscles, but not the maximum isometric
49 torque, can predict the maximum recoverable lean angle.

50

51 **Key words:** Balance recovery; Rate of torque development; Maximum isometric torque;
52 Maximum recoverable lean angle

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54

1. Introduction

55

56 The ability to step forward rapidly with the lower limb plays an important role in
57 preventing a fall after forward loss of balance (Van Dieën, Pijnappels, & Bobbert, 2005).
58 In the tether-release method, which is used to investigate step recovery in fall avoidance,
59 the subject is placed in a forward inclined position with hips pulled backwards (Hsiao-
60 Weckler, 2008). Individuals who can recover their balance in a single step from a
61 maximum initial forward leaning position, known as the maximum recoverable lean angle,
62 have a better ability to recover balance (Thelen, Wojcik, Schultz, Ashton-Miller, &
63 Alexander, 1997). Several previous studies using the tether-release method revealed that
64 older adults have less maximum recoverable lean angle compared to young individuals
65 (Hsiao-Weckler & Robinovitch, 2007; Madigan & Lloyd, 2005; Thelen et al., 1997;
66 Wojcik, Thelen, Schultz, Ashton-Miller, & Alexander, 1999). Additionally, older adults
67 are more likely to use multiple steps to recover balance as the initial forward lean angle
68 increases (Carty et al., 2015; Carty, Barrett, et al., 2012; Carty, Cronin, Lichtwark, Mills,
69 & Barrett, 2012). In older adults, the use of multiple steps to recover balance during tether-
70 release experiments is a predictor of future fall events (Carty et al., 2015).

71 Several studies have attempted to predict the maximum recoverable lean angle or
72 magnitude using the maximum joint torque of the lower limb. In a study of young and
73 older adults, isometric torques of hip flexion and ankle plantarflexion were not good
74 predictors of maximum recoverable lean angle (Wojcik, Thelen, Schultz, Ashton-Miller,
75 & Alexander, 2001). In contrast, other studies showed that the maximal isometric joint

76 torques of ankle plantarflexion and knee extension could predict the margin of stability in
77 young and older adults (Karamanidis, Arampatzis, & Mademli, 2008). Furthermore, ankle
78 dorsiflexion torque is also a weak predictor of balance recovery in older adults (Grabiner,
79 Owings, & Pavol, 2005). In a recent study (Graham, Carty, Lloyd, & Barrett, 2015)
80 amongst community-dwelling older adults, which used a stepwise multiple regression to
81 analyze maximal recoverable lean magnitude as the independent variable, some joint
82 moments and powers in the stepping leg during balance recovery were extracted as
83 explanatory variables, whereas isometric joint torques were not. These studies have all
84 measured maximum joint torques of the lower limb using an isokinetic dynamometer.
85 Thus, it is not clear if maximum joint torques is a good predictor of maximum recoverable
86 lean angle. Balance recovery requires the timely generation of appropriate joint moment
87 and muscle power to step forward quickly (Aragão, Karamanidis, Vaz, & Arampatzis,
88 2011; Arampatzis, Peper, & Bierbaum, 2011; Madigan, 2006); thus, apart from muscle
89 strength, explosive force was also thought to be necessary for rapid stepping.

90 The relationship between the maximum recoverable lean angle and maximum
91 isometric torque of the lower limb has been frequently investigated, whereas the rate of
92 torque development (RTD), which is the rate at which torque production occurs, has not
93 been investigated. The characteristics of RTD are inconsistent during contraction. A
94 relatively early-phase RTD within the first 100 ms of a rapid contraction shows great
95 variability between different individuals (Folland, Buckthorpe, & Hannah, 2014), while a
96 late-phase RTD of a longer duration (100-250 ms) has a strong correlation with maximum
97 muscle strength (Andersen & Aagaard, 2006). The early phase of RTD is related to

98 neuronal factors like individual motor unit discharge rate. Since this is the chief force-
99 generating capacity in an explosive situation, it likely plays an important role in fall
100 avoidance (Maffiuletti et al., 2016).

101 The aim of this pilot study was to investigate the correlation between the maximum
102 recoverable lean angle, using the tether-release method with maximum torque, and RTD
103 in each phase and each joint of the stepping limb. Fall avoidance relies on production of
104 adequate voluntary muscle strength in a short period of time. In addition, achieving
105 balance recovery from a larger initial lean angle requires faster joint velocity (Madigan &
106 Lloyd, 2005) and greater muscular activity (Thelen et al., 2000). We hypothesized that
107 early RTD will be a better predictor of maximum recoverable lean angle than late RTD or
108 maximum isometric torque of the lower limbs.

109

110

2. Methods

111

2. 1. Participants

112 The participants comprised 56 untrained healthy young adults (28 men; mean age,
113 21.0 ± 0.8 years; height, 1.70 ± 0.05; weight, 62.1 ± 7.2 kg; 28 women; mean age, 21.1 ±
114 0.8 years; height, 1.55 ± 0.06; weight, 49.0 ± 4.7 kg). People with orthopedic disorders
115 that would impede fall-avoidance stepping performance were excluded. Furthermore,
116 targeted participants were free of upper and lower limb pain and discomfort. G*Power
117 (ver. 3.1.9.2) was used to determine the sample size. To calculate the sample size of a
118 multiple regression analysis, we used Cohen's f^2 for effect size, set at 0.35 (representing
119

120 a large effect) and at an alpha level of 0.05 and power of 0.80. The number of predictors
121 was set at 30, as RTD consists of 6 joint movements and 5 time points. Based on the above
122 assumptions, a minimum of 36 participants were required for this study. The study was
123 approved by the Seijoh University Ethics Committee (Approval Number: 16PT07) and
124 informed consent was obtained from all participants who received sufficient explanation
125 about the research objectives and methods.

126

127 2. 2. Experimental procedures

128 2. 2. 1. Measurements of maximum recoverable lean angle

129 Participants were fitted with a harness (Full harness EHC-9A, Sanko, Inc., Japan)
130 and a tether was attached at the posterior lumbar L1-L2 level. The tether release switch, a
131 customized car seatbelt buckle, was fixed to a metal strut that permitted height adjustment
132 behind the subject. While tethered, with arms folded the chest, the participants adopted a
133 forward inclined ready-position with legs placed horizontally and shoulder-width apart. A
134 Chapman dominant leg test (Chapman, Chapman, & Allen, 1987) was performed, and the
135 leg that used for stepping during the fall was defined as the dominant or stepping leg.
136 Participants were instructed in advance to use their dominant leg during the stepping
137 movement. Reflective markers were attached to the acromion and lateral malleolus on the
138 stepping-leg side. An optical, high-speed camera synchronized to a personal computer was
139 installed at a position 2 m lateral to the stepping-leg side. The camera frame rate was 240
140 fps. Participants were instructed to keep their back straight in the forward inclined position
141 prior to tether release. The forward inclination angle (Hsiao-Weckslar & Robinovitch,

142 2007) between the axis perpendicular to the floor and the line connecting the acromion
 143 and lateral malleolus markers on the stepping-leg side was derived using a free imaging
 144 analysis software (ImageJ, version 1.44). For safety, a cushioned mat was placed 2 m in
 145 front of the subject.

146 Participants were instructed to quickly move their stepping leg forward at the instant
 147 the tether was released and limit this movement to 1 step. Forward inclination angle was
 148 increased by 5° increments starting from 15° until single-step balance recovery was no
 149 longer possible, or a portion of their body touched the cushioned mat in front of them.
 150 After failing twice in the single step balance recovery, the forward inclination angle was
 151 then reduced by 2° increments until balance recovery was again successful twice, which
 152 was defined as the maximum recoverable lean angle.

153

154 2. 2. 2. Torque measurements

155 A hand-held dynamometry (HHD) (Mobie MT-100, SAKAImed, Japan) and pull
 156 sensor (MT-150, SAKAImed, Japan) were used for torque measurements of flexion and
 157 extension in the hip, knee, and ankle (Fig. 1). The device senses and measures force by
 158 pulling a distortion gauge, and joint torque can be measured with a fixation to the non-
 159 elastic belt (Suzuki, 2015). Hence, the HHD with external fixation was used in this study
 160 so that the examiner is not required to hold the HHD. The lower limb of the stepping side
 161 during balance recovery tasks (i.e., dominant leg) was measured. The positions of the
 162 joints for each of the force measurements by the HHD are shown in Fig. 1. Limb position
 163 and the belt with pull sensor installation locations (i.e., points of resistance) were based

164 on the methods of Thorborg et al. (2013), Koblbauer et al. (2011), and Moraux et al. (2013)
165 for measurements involving the hip, knee, and ankle dorsiflexion, respectively. The
166 participants were seated on a plinth adjustable to their height in an upright position and
167 their hips and knees were positioned at approximate right angles. The joint angles were
168 measured with a goniometer based on the body landmark (e.g., line connecting the greater
169 trochanter, knee joint center, lateral malleolus) in the testing positions. The belt with pull
170 sensor was positioned distally on the thigh, distally on the anterior aspect of the tibia,
171 distally on the posterior calf complex, and on top of the foot at the level of the metatarsal,
172 for hip flexion, knee extension, knee flexion, and ankle dorsiflexion, respectively. For hip
173 extension, the belt was positioned at the posterior calf-complex with participants in a
174 prone position. Ankle plantarflexion torque had to be measured with knee extension,
175 because the stepping reaction from a forward fall required a push-off in the knee extension
176 position. Specifically, for ankle plantarflexion, the participants were positioned directly
177 on an isokinetic joint torque measuring device in a long sitting position with hips flexed
178 at 70°, knees extended at 0°, trunk and thighs fixed, and the belt with pull sensor installed
179 between the planta and the ankle plate. To ensure muscular contraction without joint
180 movement, the belt with the pull sensor was tautened to keep the limb in the torque
181 measurements position. The length of the lever arm, which spanned the distance between
182 the center of the joint and the point of effort, i.e., the location of the belt with pull sensor,
183 was recorded for each subject in all measurements. A previous study has reported that the
184 rate of force development measured using the HHD has a high reliability (Mentiplay et
185 al., 2015).

186

187

+++++ Include Figure 1 here +++++

188

189 Participants performed a sufficient warm-up and three rounds of practice trials with
190 moderate effort before measurement. To calculate the isometric maximum joint torque and
191 RTD of these joint movements, participants were instructed to quickly exert maximum
192 isometric joint torque when a signal was given by the examiner. Strong verbal
193 encouragement was provided during each joint torque measurements to promote maximal
194 effort. Force values were continuously recorded at a sampling rate of 1.5 kHz using the
195 Myoresearch version 2.1 (Noraxon USA, Inc., Scottsdale, AZ). Each joint movement was
196 successively measured three times.

197

198 2. 3. Data analyses

199 Force data were band-pass filtered at 20–500 Hz with second-order Butterworth
200 characteristics, and multiplied by lever-arm length and divided by subject body weight to
201 derive a normalized torque-time curve. Maximum joint torque was defined as normalized
202 torque-time curve peak values (Nm/kg). The average value of three maximal joint torque
203 was adopted used for the final analyses.

204 The time of torque onset was defined as the moment when the HHD reading
205 exceeded three standard deviations (SD) below the average value during the 500 ms before
206 force exertion, based on the methods of de Ruitter, Kooistra, Paalman, and de Haan (2004).
207 In addition, onset was visually verified for each subject. The slope of the torque-time

208 curve was calculated (Nm/kg/s) from onset with every 50 ms interval up to 250 ms, named
209 RTD_{0-50} , RTD_{0-100} , RTD_{0-150} , RTD_{0-200} , and RTD_{0-250} . The average value of three RTDs for
210 each time point was used for the final analyses.

211

212 2. 4. Statistical processing

213 The normality of all data was examined with the Shapiro-Wilk test. All data,
214 including the maximum joint torques, each time point of RTD, and the maximum
215 recoverable lean angle, were normally distributed. The intra-rater reliability of the
216 maximum joint torque and RTD at each time point among three measurements was
217 estimated using intra-class correlation coefficients (ICC). Pearson's product moment
218 correlations assessed the relationships between maximum recoverable lean angle and each
219 time point on RTD-dependent variables. The Pearson product moment correlations were
220 presented for all RTD at each time point and maximum joint torque, and multicollinearity
221 was verified prior to multiple regression analyses. If the correlation coefficient between
222 the two RTD in the same joint movement exceeded 0.80, the later RTD was excluded from
223 the explanatory variables. Multiple stepwise regression analyses were performed using
224 maximum recoverable lean angle as the independent variable and lower-limb maximum
225 joint torque and each time point on RTD as explanatory variables. The statistical
226 significance threshold was set at 5%.

227

228 3. Results

229

230 The ICCs for the maximum joint torque ranged from 0.90 to 0.96 for each targeted
231 joint movement. Additionally, the ICCs for the RTD at each time point and among targeted
232 joint movements are provided in Table 1. Although early RTD (≥ 100 ms) for some joint
233 movements exhibited a lower value compared with late RTD, these ICC results indicated
234 substantial to almost perfect reliability (Landis & Koch, 1977).

235

236 **+++++ Include Table 1 here +++++**

237

238 The average \pm SD for maximum recoverable lean angle was $32.4 \pm 5.1^\circ$ in all
239 participants. Maximum joint torque and RTD data at each time point are shown in Table
240 2. A significant positive correlation was observed for the maximum recoverable lean angle
241 with hip flexion ($r = 0.561$, Cohen's $f^2 = 0.46$), hip extension ($r = 0.301$, Cohen's $f^2 = 0.10$),
242 knee flexion ($r = 0.341$, Cohen's $f^2 = 0.13$), ankle plantarflexion ($r = 0.334$, Cohen's $f^2 =$
243 0.13), and ankle dorsiflexion ($r = 0.538$, Cohen's $f^2 = 0.41$) by maximum joint torque. As
244 shown in Table 3, a significant positive correlation was observed for RTD of each time
245 point on several of these. All the hip flexion RTDs at each time point showed a significant
246 relationship, while significant relationships were not found for all the knee extension
247 RTDs at each time point.

248

249 **+++++ Include Table 2 and Table 3 here +++++**

250

251 The RTD_{0-200} , RTD_{0-250} , and maximal joint torque in all joint movements had a

252 correlation coefficient of more than 0.80. This means that the maximum torque and RTD₀₋
253 ₂₀₀ and RTD₀₋₂₅₀ were strongly correlated. Therefore, RTD₀₋₂₀₀ and RTD₀₋₂₅₀ were
254 excluded from the explanatory variables to avoid multicollinearity. Instead, the
255 maximum joint torque was included. Multiple stepwise regression analysis showed that
256 hip flexion RTD₀₋₅₀, knee flexion RTD₀₋₁₀₀, and hip flexion RTD₀₋₁₅₀ (adjusted R²= 0.589,
257 F= 27.27, p< 0.001) were the best predictors of maximum recoverable lean angle (Table
258 4).

259

260 **+++++ Include Table 4 here +++++**

261

262

4. Discussion

263

264 To the best of our knowledge, this is the first study to examine the relationship between
265 the maximum recoverable lean angle created by the tether-release method and RTD for
266 the lower limb. Our results support our hypothesis that early-phase RTD predicts the
267 maximum recoverable lean angle better than maximum isometric torque. Maximum
268 recoverable lean angle was correlated with maximum isometric torque and RTD for some
269 joint movements, but not knee extension in the single regression analysis. A stepwise
270 multiple regression analysis involving RTD less than 200 ms and maximal joint torque
271 showed that hip flexion RTD₀₋₅₀ and RTD₀₋₁₅₀ as well as knee flexion RTD₀₋₁₀₀ were
272 predictors of maximum recoverable lean angle, as opposed to maximum isometric torque.
273 Additionally, the standard partial regression coefficient displayed a stronger effect in the

274 RTD₀₋₅₀ and RTD₀₋₁₀₀ of the hip and knee flexion than the RTD₀₋₁₅₀ of hip flexion.

275 Single regression analysis showed that the maximum isometric torque, excluding
276 knee extension, significantly correlated with maximum recoverable lean angle. The effect
277 of maximum muscle strength on RTD increases with time from the onset of contraction;
278 particularly as RTD₀₋₂₀₀ has a strong correlation with maximum muscle strength (Andersen
279 & Aagaard, 2006). This may explain our results indicating that the maximum isometric
280 torque, excluding knee extension, and RTD₀₋₂₀₀ and RTD₀₋₂₅₀ in the same joint movement
281 were both significantly correlated with the maximum recoverable lean angle. Although
282 there were significant positive correlations in most of the joint movements, none were
283 chosen as predictors of maximum isometric joint torque in the stepwise multiple
284 regression analysis. Maximum available torques in the stepping leg were not used during
285 the balance recovery from tether-release in younger adults (Graham, Carty, Lloyd,
286 Lichtwark, & Barrett, 2014; Wojcik et al., 2001). Therefore, as an individual's maximum
287 torque level does not directly relate to the balance recovery capacity, isometric maximum
288 joint torque is only at most a moderate predictor of maximum recoverable lean angle.

289 Reduced postural stability during upright standing in older adults is related to
290 decreased leg extension rate of force development (Izquierdo, Aguado, Gonzalez, López,
291 & Häkkinen, 1999). Decreased production of explosive force might affect the time until
292 neuromuscular response during balance recovery. The muscle reaction time for the
293 stepping limb in tether release was within 80 ms (Thelen et al., 2000). Therefore, early
294 RTD of lower limb joint torque is likely involved in impulsive situations such as fall
295 avoidance. In fact, early RTD, namely the RTD₀₋₅₀ of hip flexion and the RTD₀₋₁₀₀ of knee

296 flexion, were extracted as predictors of the maximum recoverable lean angle in this study.
297 It has been reported that early RTD is predominantly dependent on muscular activation
298 levels at the onset of the contraction (de Ruitter et al., 2004). Recruiting a larger proportion
299 of the available motor units is required to achieve a large and rapid stepping movement
300 during balance recovery (Cronin, Barrett, Lichtwark, Mills, & Carty, 2013). The lower
301 rate of development for muscle activation has been shown to lead to decreased rate of
302 force generation in the lower leg, resulting in an inadequate recovery response and
303 increased fall risk (Pijnappels, Bobbert, & Van Dieën, 2005). The hip flexion and knee
304 flexion torques, chosen as predictive variables in the current study, work in
305 the early phase during the tether release step, and contribute to forward
306 progression and knee flexion in the stepping limb (Madigan, 2006). The rate of
307 hip flexion moment generation during balance recovery is related to the
308 maximum recoverable lean angle magnitude for tether-release (Arampatzis et
309 al., 2011). Another study also reported that the semitendinosus peak muscular
310 activity contributing to knee flexion was significantly associated with step
311 length during balance recovery (Cronin et al., 2013). The relationships between
312 the balance recovery capacity and the lower limb early RTD in the current study may be
313 indirectly related to the ability to execute large and rapid steps.

314 In a previous study of lower limb torques measured by an isokinetic dynamometer
315 and a simple linear regression analysis of balance recovery, the margin of stability for
316 joint torques of the ankle plantarflexion and knee extension were predicted as 44% and
317 35%, respectively (Karamanidis et al., 2008), and ankle dorsiflexion torque predicted

318 maximum recoverable lean angle in older adults at a rate of 30% (Grabiner et al., 2005).
319 Moreover, ankle plantarflexion and hip flexion muscle strength predicted the maximum
320 recoverable lean magnitude at contribution rates of 18% and 19%, respectively (Graham
321 et al., 2015). Although this study of healthy young volunteers differs from the studies that
322 included older adults, the RTD_{0-50} of hip flexion and RTD_{0-100} of knee flexion, and the
323 RTD_{0-150} of hip flexion that were measured by a HHD predicted the maximum recoverable
324 lean angle at a multiple coefficient of determination of 59%. The comprehensive analysis
325 including maximum isometric torque of the lower limbs and RTD in this study
326 demonstrated that maximum recoverable lean angle can be predicted. The relationship
327 between explosive force and maximum recoverable lean angle, including kinematic
328 analysis of older adults, needs to be investigated in the future.

329 When interpreting the results of the present study, caution is needed regarding the
330 following limitations. First, since the joint angles at peak contraction was not confirmed,
331 participants may have been allowed a slight movement of the joint during the explosive
332 maximum torque measurement, with the exception of ankle plantarflexion. Participants
333 kept the limb position with the HHD belt taut at the position in which maximum torque
334 was produced. This could cause slight muscular activation, which might have affected
335 maximum joint torque. Nevertheless, the RTD at each time point and each joint had
336 moderate to high reproducibility even if there are limitations of the method used for joint
337 torque measurements in the current study. Second, the joint torque measurements used
338 were isometric contractions and do not reflect the joint angular speed pertinent to balance
339 recovery stepping. Third, although there may be a gender difference in magnitude of joint

340 torques used for balance recovery stepping (Wojcik et al., 2001), the regression analysis
341 in the current study included men and women. Lastly, as no kinesiologic or
342 electromyographic analysis of the tether-release method was conducted, it remains unclear
343 how the participants' joint strength contributed, or how muscle co-activations or
344 coordination of contraction timing may have affected balance recovery. Forward balance
345 loss recovery was accomplished by adequate trunk regulation, lower limb moment
346 generation, power, and a long and rapid step (Graham et al., 2015). Accordingly, we agree
347 that predictor variables for maximum recoverable lean angle, including kinematic analysis
348 of tether release stepping must be determined. In particular, it is necessary to clarify the
349 explosive force of lower limbs that contributes to the expansion of the step length from
350 the maximum recoverable lean angle.

351

352

5. Conclusion

353

354 RTD measurement using the HHD is a predictive factor for maximum recoverable lean
355 angle in the tether-release test. Additionally, hip flexor RTD₀₋₅₀, RTD₀₋₁₅₀, and knee flexor
356 RTD₀₋₁₀₀ were related to 59% of the shared variance of maximum recoverable lean angle.
357 The findings of the present study suggest that early-phase RTD for a portion of the lower
358 limb, rather than maximum isometric torque, can predict maximum recoverable lean angle
359 in healthy young adults.

360

361 **Conflict of interest statement**

362 None of the authors report a conflict of interest.

363

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Figure 1.

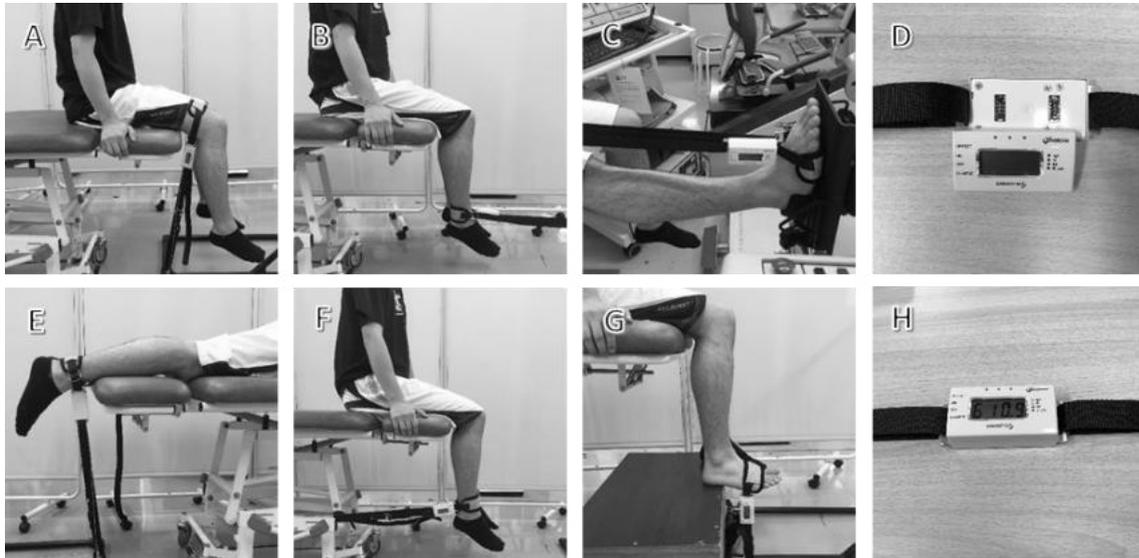


Figure title and caption

Figure 1: Testing positions for force measurements for the dynamometer and belt with pull sensor.

The belt with the pull sensor was fixed to the metal base frame placed on the floor for hip flexion (A), hip extension (E), and ankle dorsiflexion (G). The belt was also externally fixed to the vertical metal bar or a plinth frame for knee flexion (B) or knee extension (F), respectively. For the measurements of ankle plantar flexion force (C), the belt with pull sensor was fixed to the seat frame of the isokinetic joint torque measuring device to be straight along the long axis of the lower leg. The belt with the pull sensor and hand-held dynamometry (D), and the device in action (H).

Table 1

Table 1. Intra-class correlation coefficients for the maximum joint torques and rate of torque development at each time point.

	Peak torque	RTD ₀₋₅₀	RTD ₀₋₁₀₀	RTD ₀₋₁₅₀	RTD ₀₋₂₀₀	RTD ₀₋₂₅₀
HF	0.90 (0.85-0.94)	0.81 (0.71-0.89)	0.83 (0.73-0.89)	0.86 (0.79-0.92)	0.86 (0.78-0.91)	0.87 (0.79-0.92)
HE	0.95 (0.92-0.97)	0.77 (0.64-0.86)	0.82 (0.73-0.89)	0.83 (0.74-0.90)	0.92 (0.87-0.95)	0.87 (0.80-0.92)
KF	0.96 (0.94-0.98)	0.82 (0.71-0.89)	0.86 (0.78-0.91)	0.83 (0.74-0.90)	0.94 (0.90-0.96)	0.93 (0.89-0.96)
KE	0.91 (0.86-0.94)	0.74 (0.60-0.84)	0.84 (0.75-0.90)	0.83 (0.74-0.90)	0.88 (0.82-0.93)	0.89 (0.83-0.93)
APF	0.90 (0.85-0.94)	0.74 (0.59-0.84)	0.82 (0.72-0.89)	0.81 (0.70-0.88)	0.81 (0.71-0.88)	0.87 (0.79-0.92)
ADF	0.92 (0.87-0.95)	0.73 (0.57-0.83)	0.82 (0.73-0.89)	0.87 (0.80-0.92)	0.93 (0.89-0.96)	0.90 (0.84-0.94)

These data were shown in the ICCs (95% confidence intervals from lower bound to upper bound).

HF, hip flexion; HE, hip extension; KF, knee flexion; KE, knee extension; APF, ankle plantarflexion; ADF, ankle dorsiflexion.

Table 2

 Table 2. Mean lower limb maximum joint torques and rate of torque development at each time point (mean \pm standard deviation).

	Maximum joint torque	RTD ₀₋₅₀	RTD ₀₋₁₀₀	RTD ₀₋₁₅₀	RTD ₀₋₂₀₀	RTD ₀₋₂₅₀
HF	1.46 \pm 0.29	9.71 \pm 4.07	8.92 \pm 3.14	5.76 \pm 1.67	5.66 \pm 1.24	4.53 \pm 0.91
HE	1.42 \pm 0.38	10.09 \pm 4.43	9.16 \pm 3.05	5.80 \pm 1.65	5.62 \pm 1.62	4.38 \pm 1.14
KF	1.42 \pm 0.41	9.81 \pm 4.88	8.75 \pm 3.32	5.70 \pm 1.84	5.49 \pm 1.64	4.40 \pm 1.31
KE	2.44 \pm 0.53	16.66 \pm 6.62	15.76 \pm 4.84	10.17 \pm 2.63	9.52 \pm 2.20	7.55 \pm 1.70
APF	1.04 \pm 0.19	7.27 \pm 3.07	6.48 \pm 2.18	4.14 \pm 1.00	4.04 \pm 0.73	3.26 \pm 0.61
ADF	0.49 \pm 0.15	3.59 \pm 1.53	3.25 \pm 1.26	1.94 \pm 0.68	1.89 \pm 0.58	1.51 \pm 0.46

Each time point RTD was calculated at all time points starting from onset at every 50 ms interval. The unit for maximum joint torques were “Nm/kg”, and RTDs were “Nm/kg/s”. HF, hip flexion; HE, hip extension; KF, knee flexion; KE, knee extension; APF, ankle plantarflexion; ADF, ankle dorsiflexion.

Table 3

Table 3. Coefficients of correlation based on a single variable linear correlation analysis between maximum joint torques and rate of torque development at each time point and maximum recoverable lean angle

		Maximum torque	RTD ₀₋₅₀	RTD ₀₋₁₀₀	RTD ₀₋₁₅₀	RTD ₀₋₂₀₀	RTD ₀₋₂₅₀
HF	r	0.561 **	0.587 **	0.635 **	0.560 **	0.510 **	0.473 **
	ES	0.46	0.53	0.68	0.46	0.35	0.29
HE	r	0.301 *	0.142	0.407 **	0.285 *	0.329 *	0.345 **
	ES	0.10	0.02	0.20	0.09	0.12	0.14
KF	r	0.341 *	0.540 **	0.543 **	0.197	0.307 *	0.353 **
	ES	0.13	0.41	0.42	0.04	0.10	0.14
KE	r	0.237	0.237	0.128	0.095	0.141	0.132
	ES	0.06	0.06	0.02	0.01	0.02	0.02
APF	r	0.334 *	0.428 **	0.516 **	0.220	0.331 *	0.352 **
	ES	0.13	0.22	0.36	0.05	0.12	0.14
ADF	r	0.538 **	0.160	0.157	0.252	0.381 **	0.401 **
	ES	0.41	0.03	0.03	0.07	0.17	0.19

A significant correlation was denoted by * = $p < 0.05$, and ** = $p < 0.01$.

HF, hip flexion; HE, hip extension; KF, knee flexion; KE, knee extension; APF, ankle plantarflexion; ADF, ankle dorsiflexion; ES, effect size given by Cohen's f^2

Table 4

Table 4. Result of multiple stepwise regression analysis for predicting maximum recoverable lean angle.

Variable	B	95% CI	SE	Beta	T	P
Model: $R^2= 0.589$, $F= 27.27$, $p < 0.001$						
HF RTD ₀₋₅₀	0.443	0.163-0.724	0.140	0.353	3.172	0.003
KF RTD ₀₋₁₀₀	0.574	0.289-0.859	0.142	0.373	4.046	< 0.001
HF RTD ₀₋₁₅₀	0.863	0.190-1.536	0.336	0.282	2.572	0.013

HF, hip flexion; KF, knee flexion; RTD, rate of torque development; B, unstandardized coefficients of B; 95%CI, 95% confidence interval for B and lower bound to upper bound; SE, standard error; Beta, standardized coefficients of Beta; T, t value; P, p value